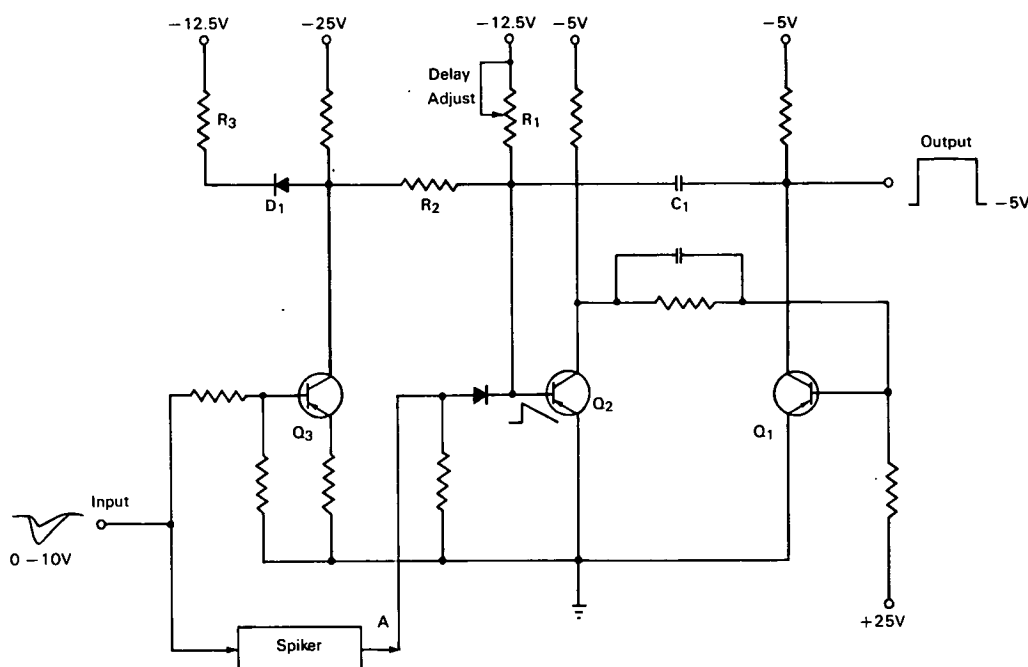


# AEC-NASA TECH BRIEF



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## Modified Univibrator Compensates for Output Timing Errors



### The problem:

To design a univibrator circuit capable of time-synchronizing the trailing edge of the output pulse with the origin of the input pulse. Conventional univibrator circuits are subject to output pulse timing errors produced by varying input pulse amplitudes.

### The solution:

A simple, one-stage, delay compensation amplifier, added to the conventional univibrator circuitry so as to produce a univibrator output pulse whose trailing edge is independent of the amplitude of the input pulse.

### How it's done:

The timing circuit consists of conventional univibrator  $Q_1$  and  $Q_2$ , a spiker circuit, and one-stage compensation transistor amplifier  $Q_3$ .

In the quiescent state,  $Q_2$  is conducting;  $Q_1$  and  $Q_3$  are biased off. An input pulse is applied simultaneously to the spiker circuit and to the base of  $Q_3$ . The spiker applies a positive spike to the base of  $Q_2$ , switching it off. When  $Q_2$  stops conducting, sufficient current flows to the base of  $Q_1$  to bias it into the conduction region.  $Q_1$  turns on and generates a positive-going output pulse.  $Q_2$  is held in the cut-off state by

(continued overleaf)

the potential across capacitor  $C_1$  and remains biased off until  $C_1$  is sufficiently discharged.

In a conventional univibrator, the discharge of  $C_1$  is governed by the current flowing through  $R_1$ . However, in the compensated univibrator, the discharge of  $C_1$  is governed by a discharge path through both  $R_1$  and  $R_2$ . The potential existing at point A determines the discharge current through  $R_2$ .

An input pulse drives  $Q_3$  into a state of increasing conduction, causing the point A potential to increase from  $-22\text{v}$  to the clamp potential of  $-12.5\text{v}$ . This decreases the discharge current flowing through  $R_2$ . From the time the clamp potential is reached to the end of the discharge, the discharge rate of  $C_1$  is nearly constant and slower than its initial discharge rate. For high amplitude input pulses, the threshold of  $Q_3$  and the clamp potential are reached quickly. For low amplitude input pulses, the potential at point A increases less rapidly, and the nearly constant discharge rate is reached at a later time. Thus  $C_1$  discharges more rapidly for low amplitude input pulses than for high amplitude pulses, causing the compensated univibrator to turn off earlier for low amplitude input pulses than for high amplitude input pulses.

Low amplitude inputs reach the triggering threshold of  $Q_2$  later than high amplitude inputs, causing a delay in the occurrence of the leading edge of the output pulse. The discharge control of  $C_1$ , however, compensates for this delay by producing narrow output pulses for small inputs and wide output pulses for large inputs. This pulse width compensation effect causes the trailing edge of all output pulses to occur at the same time regardless of input pulse amplitude.

#### Notes:

1. Manual adjustment of  $R_1$  determines the pulse delay time through  $C_1$  in the compensated circuit.
2. This circuit can function with double RC-differentiated input pulses and requires no delay-line wave shaping or zero crossing techniques.
3. Resistor  $R_3$  and catching diode  $D_1$  are added in the collector circuit of  $Q_3$  to enhance the compensation for input pulses of high amplitude.
4. Additional details are contained in: *The Review of Scientific Instruments*, vol. 34, no. 11, pp. 1248-1253, November, 1963.
5. Inquiries concerning this innovation may be directed to:

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#### Patent status:

Inquiries about obtaining rights for commercial use of this innovation may be made to:

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